

# Effect of the Different End Shapes on the Gain Flatness of the Antipodal Vivaldi Antenna

Öznür Türkmen-Küçüksarı<sup>1</sup>, Sibel Çimen<sup>2</sup>, and Gonca Çakır<sup>2</sup>

<sup>1</sup>Mechatronics Engineering Department, Kocaeli University, Kocaeli, Umuttepe 41380, Turkey  
oznur.kucuksari@kocaeli.edu.tr

<sup>2</sup>Electronics and Communication Engineering Department, Kocaeli University, Kocaeli, Umuttepe, 41380, Turkey  
sibelgunduz@kocaeli.edu.tr, gonca@kocaeli.edu.tr

## Abstract

In this study, effects of the different end shapes on the gain flatness of an Antipodal Vivaldi Antenna (APVA) operating over 3.1-10.6 GHz are investigated. The antenna having an ending with parallel wires is proposed for gain flatness in this study. Numerical studies are performed for four different APVAs having endings in different shapes of elliptical, circular and partially square forms and parallel wires. The best gain flatness is obtained for the antenna having the ending of the parallel wires.

## 1. Introduction

Bandwidth of 3.1-10.6 GHz was allocated for commercial UWB applications by Federal Communications Commission (FCC) in 2002. From this date, we see that studies including the antenna, filter, frequency selective surface (FSS), radar cross section reduction for communication and radar systems which operate within this frequency band have shown up rapidly in literature.

UWB antennas are foremost elements among the elements in these systems. Planar geometry, wide operating bandwidth, directive radiation pattern and high gain capability as well as small group delay and gain flatness are desired properties for UWB applications [1]-[2]. Vivaldi antennas are a prominent candidate for UWB applications. There are different versions of the Vivaldi Antenna [3]-[13]. Antipodal Vivaldi Antenna is one of these versions with simple feeding mechanism [7], [13].

In this study we focused on investigating the effect of the end shape of the antipodal Vivaldi antenna (APVA) on the gain flatness. There different antenna having end shapes in elliptical (APVA-I), circular (APVA-II) and partially rectangular (APVA-III) forms are compared to our proposed antenna having an ending with parallel wires (APVA-IV). We will show that the proposed APVA-IV provides more antenna gain flatness compared to the other antennas.

## 2. Design

A basic APVA is composed of two metallic arms as shown in Fig. 1. One of the arms is printed on the front side of a low-loss dielectric substrate. The other arm having a small ground is printed on the back side of the substrate. Outermost parts of the arms are defined by outer, inner and end curves. Equations of the inner and outer curves are in the Gaussian form as follows:

$$a(z) = \begin{cases} 19.6 \exp\left(-4\pi\left(\frac{z}{117}\right)^2\right) & -80 \leq z \leq -2 \\ \text{(inner curve)} \\ 48 \exp\left(-4\pi\left(\frac{z}{162}\right)^2\right) & -80 \leq z \leq -28.5 \\ \text{(outer curve)} \end{cases} \quad (1)$$

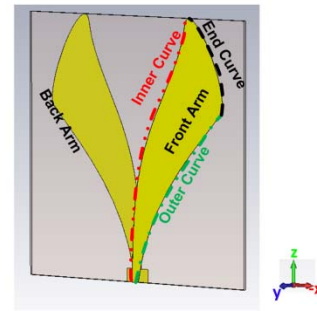


Fig. 1. Perspective view of the basic antipodal Vivaldi antenna

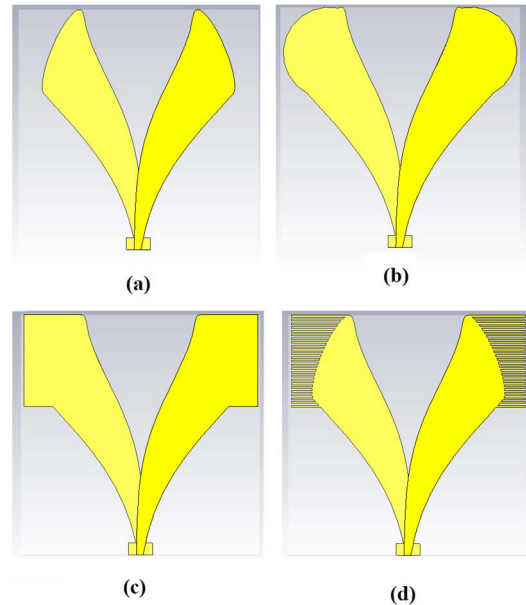


Fig. 2. Antennas with different end shaping: (a) APVA-I, (b) APVA-II, (c) APVA-III, (d) APVA-IV.

All antennas are designed using Arlon DiClad 880 square-shaped substrate of parameters side lengths  $L_s=80$  mm, permittivity  $\epsilon_r = 3$ , thickness  $d = 0.762$  mm and loss tangent  $\tan\delta = 0.009$ . Metal inclusions are made of copper with conductivity  $\sigma=5.8\times 10^7$  S/m and thickness  $t=0.035$  mm.

During the numerical trials four APVAs are designed as presented in Fig. 2. For these trials, while the other design parameters are kept constant, the shape of the end curve is only changed. For the first and second cases, the APVA-I and APVA-II have an end shape in the elliptical and circular forms as seen in Fig. 2 (a) and Fig. 2 (b), respectively. For the third case, the end curve of the antenna (called APVA-III) is turned into a shape partially wrapped around a rectangle as in Fig. 2 (c). As for the final case, the additional part which is added to the end of the APVA-I to form APVA-III is turned into the parallel wires. Design parameters of these ending parallel wires are width  $w = 0.65$  mm, gap distance  $g = 0.65$  mm.

Designed antennas are simulated by using the time domain solver of the commercial electromagnetic simulator CST Microwave Studio.

### 3. Numerical Results

Firstly, return loss,  $|S_{11}|$ , values of the antennas are given in Fig. 3 in dB.  $|S_{11}|$  curves show that all the antennas are matched to the  $50 \Omega$  source.

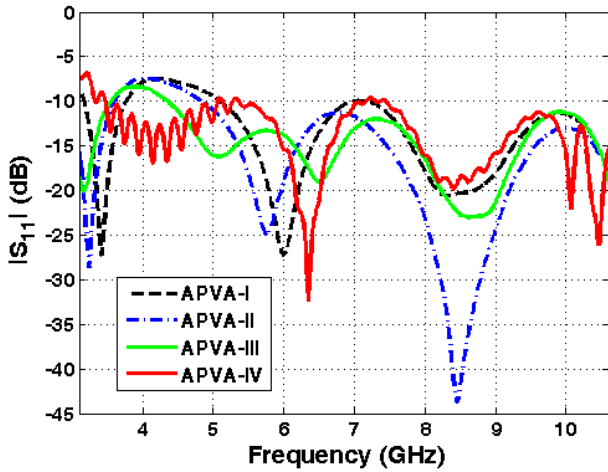


Fig. 3.  $|S_{11}|$  values of the designed antennas

Secondly, gain values of the antennas along the end-fire direction (i.e. along the  $z$  axis) over 3.1–10.6 GHz are presented in Fig. 4 in dB. The minimum and maximum gain values of the APVA-I are 2.41 dB and 11.23 dB, respectively. For APVA-II, the gain values are between 4.14 dB and 10.64 dB. As for the APVA-III the minimum and maximum gain values are 4.57 dB and 9.92 dB, respectively. For the final antenna, the APVA-IV, the highest and lowest values of the gain graph are 7.35 dB and 10.02 dB, respectively. The maximum gain deviation is 8.82 dB, 6.5 dB, 5.35 dB and 2.67 dB for APVA-I, APVA-II, APVA-III and APVA-IV, respectively. In summary, the best gain deviation is equal to 2.67 dB which is obtained for the proposed APVA-IV as seen in the Fig.4.

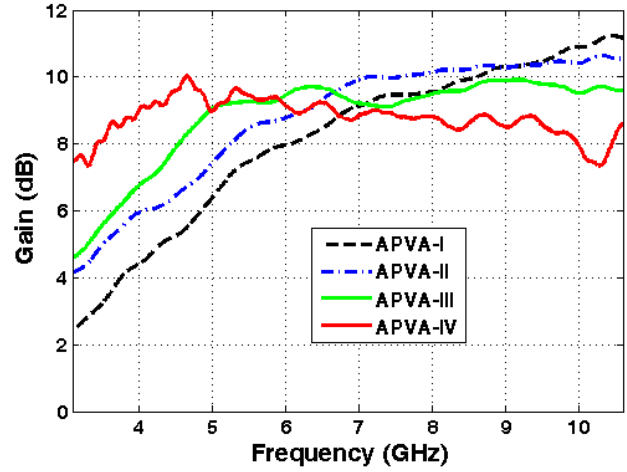


Fig. 4. Gain values of the designed antennas in dB.

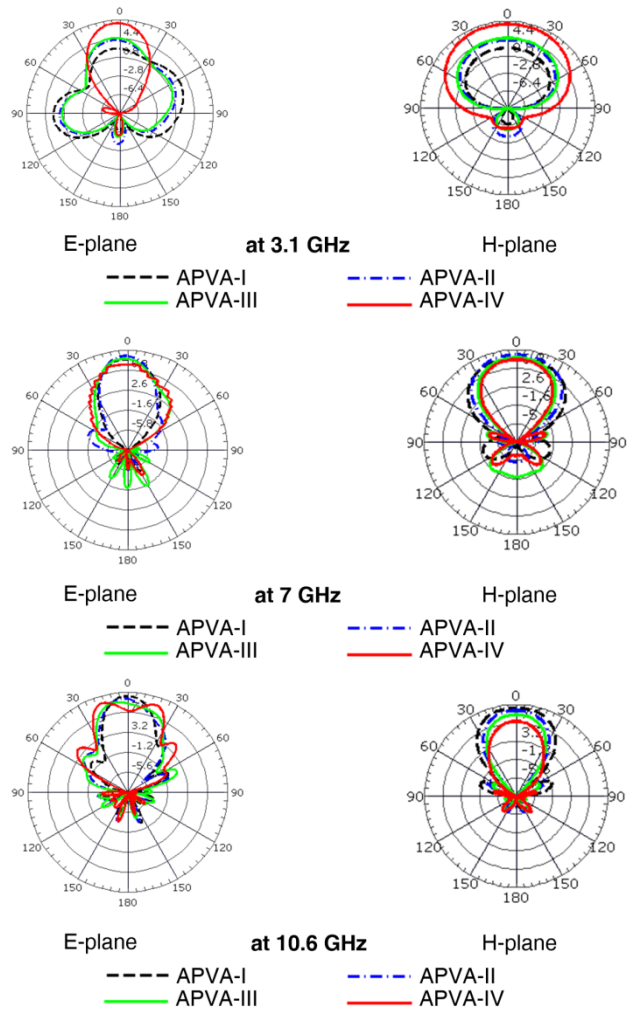
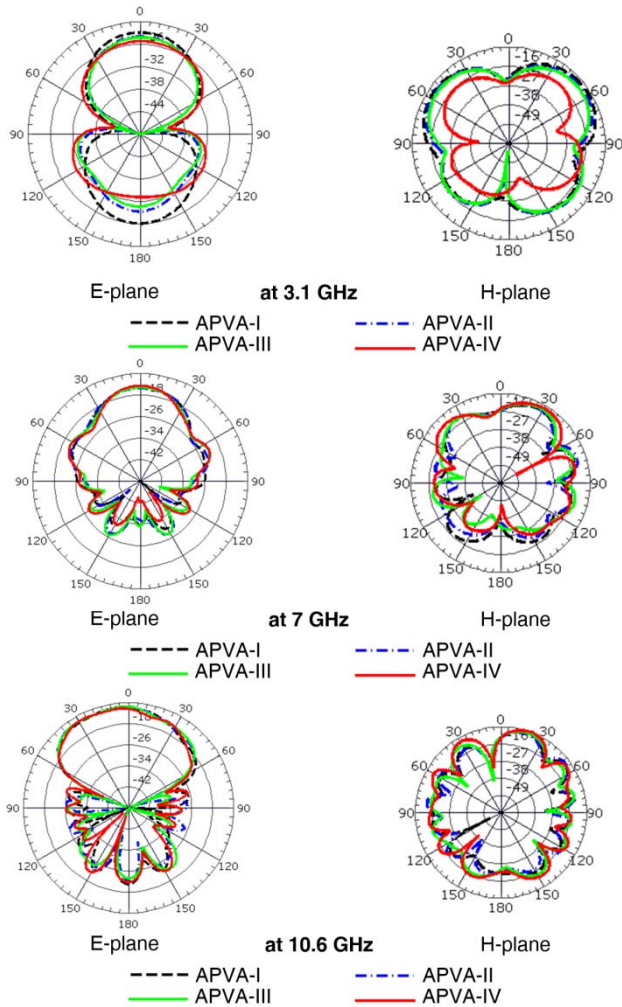


Fig. 5. Co-pol components of the gain patterns (dB) of the antennas.

Co-pol and cross-pol components of the gain patterns (dB) of the antennas are shown in Fig. 5 and Fig. 6, respectively. All the antennas have main beam directions along the end fire directions

as in Fig. 5. Higher Cross-pol levels are observed in the H plane (i.e. yz plane) patterns of all the antennas compared to their E plane (i.e. xz plane) plane patterns.



**Fig. 6.** Cross-pol components of the gain patterns (dB) of the antennas.

## 6. Conclusions

In this study we proposed a modified antipodal Vivaldi antenna having an ending with parallel wires to enhance the gain flatness of the antipodal Vivaldi antennas. Antenna gain characteristics of the different three antennas having end shapes in elliptical, circular and partially rectangular forms are compared to the proposed antenna. Numerical studies showed that the proposed APVA-IV provides more antenna gain flatness compared to the other antennas.

## 7. Acknowledgement

The authors would like to thank you The Scientific and Technological Research Council of Turkey (TUBITAK) for supporting this work (Project No: 215E101).

## 8. References

- [1] Z. N. Chen, M. J. Ammann, X. Qing, X. H. Wu, T. S. See, and A. Cai, "Planar antennas," *IEEE Microw. Mag.*, vol. 7, no. 6, pp. 63–73, 2006.
- [2] W. Wiesbeck, G. Adamiuk, and C. Sturm, "Basic properties and design principles of UWB antennas," *Proc. IEEE*, vol. 97, no. 2, pp. 372–385, Feb. 2009.
- [3] P. J. Gibson, "The vivaldi aerial," in *Microwave Conference, 1979. 9th European*, 1979, pp. 101–105.
- [4] U. Kotthaus and B. Vowinkel, "Investigation of planar antennas for submillimeter receivers," *IEEE Trans. Microw. Theory Tech.*, vol. 37, no. 2, pp. 375–380, 1989.
- [5] S. Sugawara, Y. Maita, K. Adachi, K. Mori, and K. Mizuno, "A mm-wave tapered slot antenna with improved radiation pattern," in *Microwave Symposium Digest, 1997., IEEE MTT-S International*, 1997, vol. 2, pp. 959–962.
- [6] M. C. Greenberg, K. L. Virga, and C. L. Hammond, "Performance characteristics of the dual exponentially tapered slot antenna (detsa) for wireless communications applications," *IEEE Trans. Veh. Technol.*, vol. 52, no. 2, pp. 305–312, Mar. 2003.
- [7] E. Gazit, "Improved design of the Vivaldi antenna," in *IEE Proceedings H (Microwaves, Antennas and Propagation)*, 1988, vol. 135, pp. 89–92.
- [8] J. D. S. Langley, P. S. Hall, and P. Newham, "Novel ultrawide-bandwidth Vivaldi antenna with low crosspolarisation," *Electron. Lett.*, vol. 29, no. 23, pp. 2004–2005, 1993.
- [9] E. Guillanton, J. Y. Dauvignac, C. Pichot, and J. Cashman, "A new design tapered slot antenna for ultra wideband applications," *Microwave and Optical Technology Letters*, 1998.
- [10] X. Qing, Z. N. Chen, and M. Y. W. Chia, "Dual elliptically tapered antipodal slot antenna loaded by curved terminations for ultrawideband applications: DETASA for UWB applications," *Radio Sci.*, vol. 41, no. 6, p. 1–14 (RS6009), Dec. 2006.
- [11] K. Kota and L. Shafai, "Gain and radiation pattern enhancement of balanced antipodal Vivaldi antenna," *Electron. Lett.*, vol. 47, no. 5, pp. 303–304, 2011.
- [12] J. Y. Siddiqui, Y. M. M. Antar, A. P. Freundorfer, E. C. Smith, G. A. Morin, and T. Thayaparan, "Design of an ultrawideband antipodal tapered slot antenna using elliptical strip conductors," *IEEE Antennas Wirel. Propag. Lett.*, vol. 10, pp. 251–254, 2011.
- [13] R. Natarajan, J. V. George, M. Kanagasabai, and A. Kumar Shrivastav, "A compact antipodal Vivaldi antenna for UWB applications," *IEEE Antennas Wirel. Propag. Lett.*, vol. 14, pp. 1557–1560, 2015.